



To understand Additive Manufacturing from the perspective of the Powder

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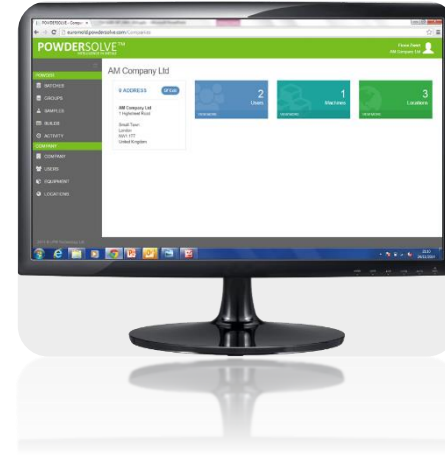
Products and Services

All focused on AM only

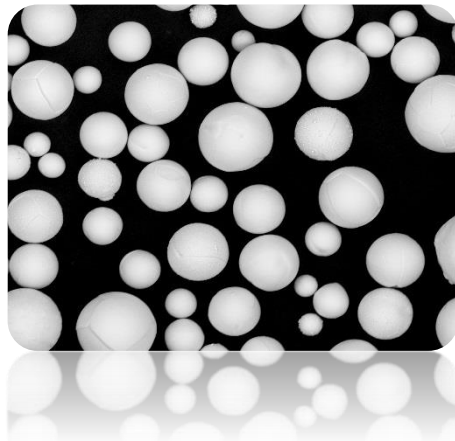
Metal Powders



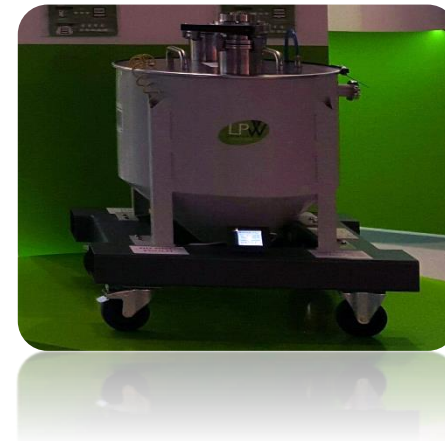
Powder Management Software



Consultancy & Lab Testing Services

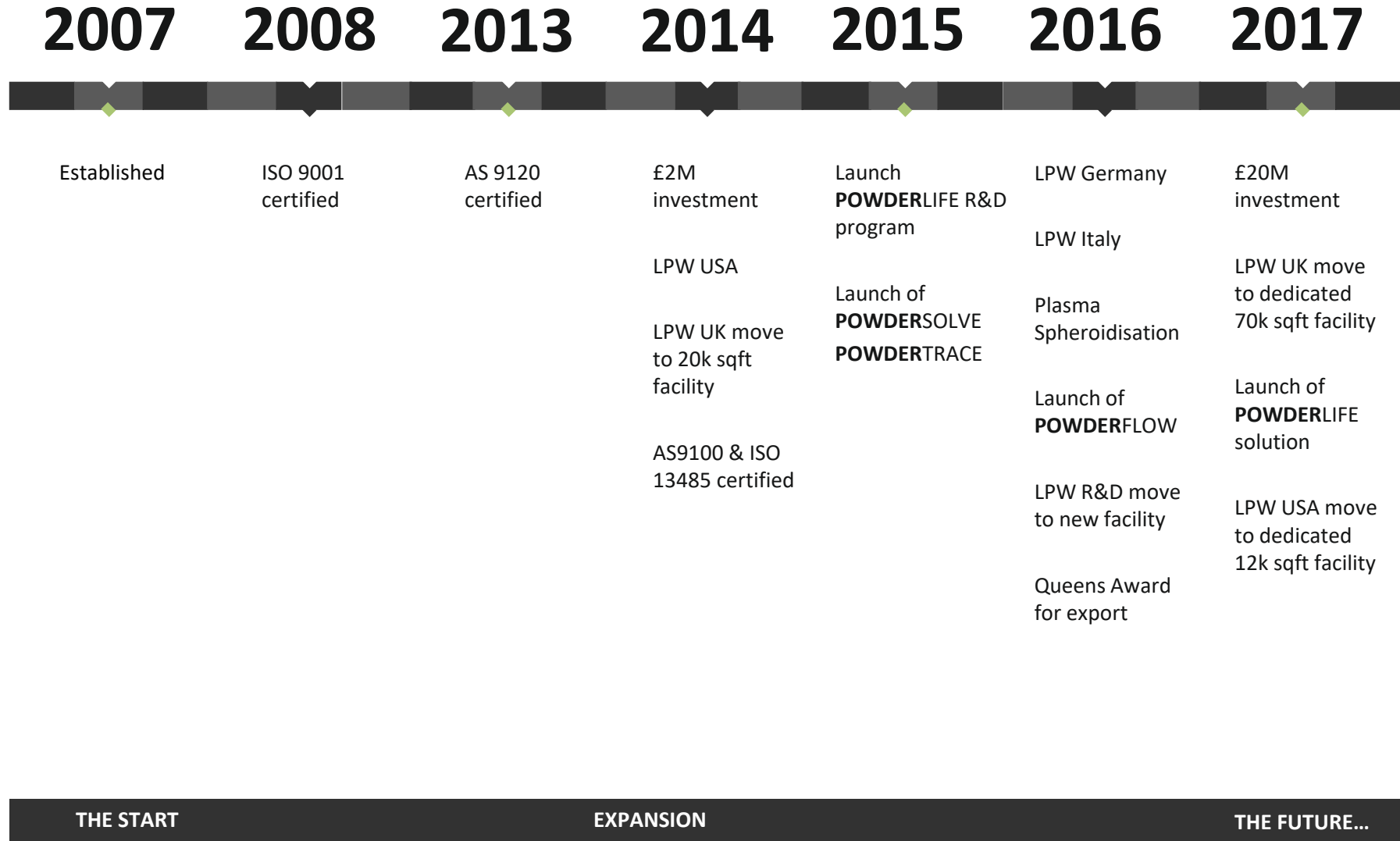


Powder Handling & Testing Equipment





LPW Development



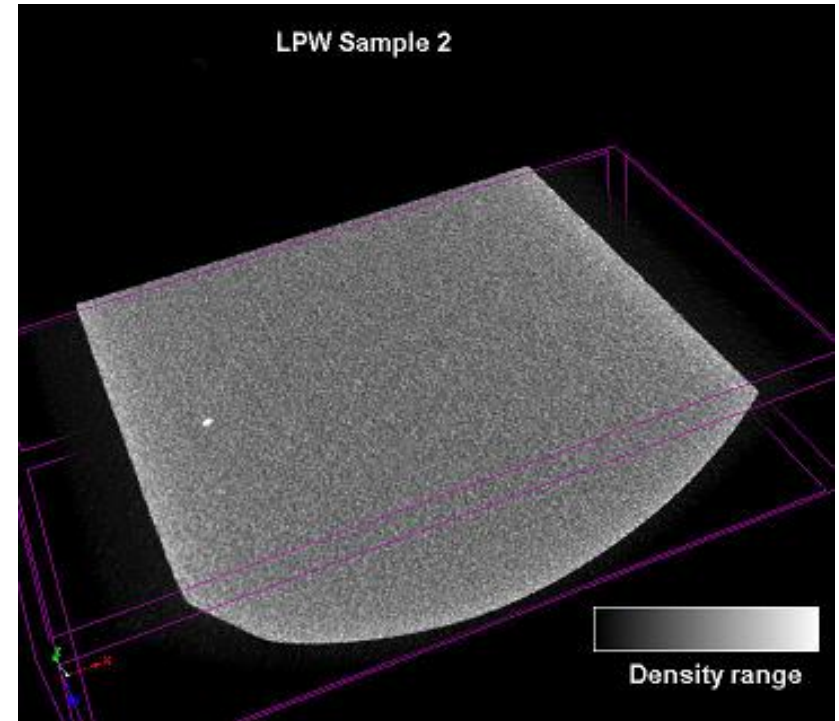
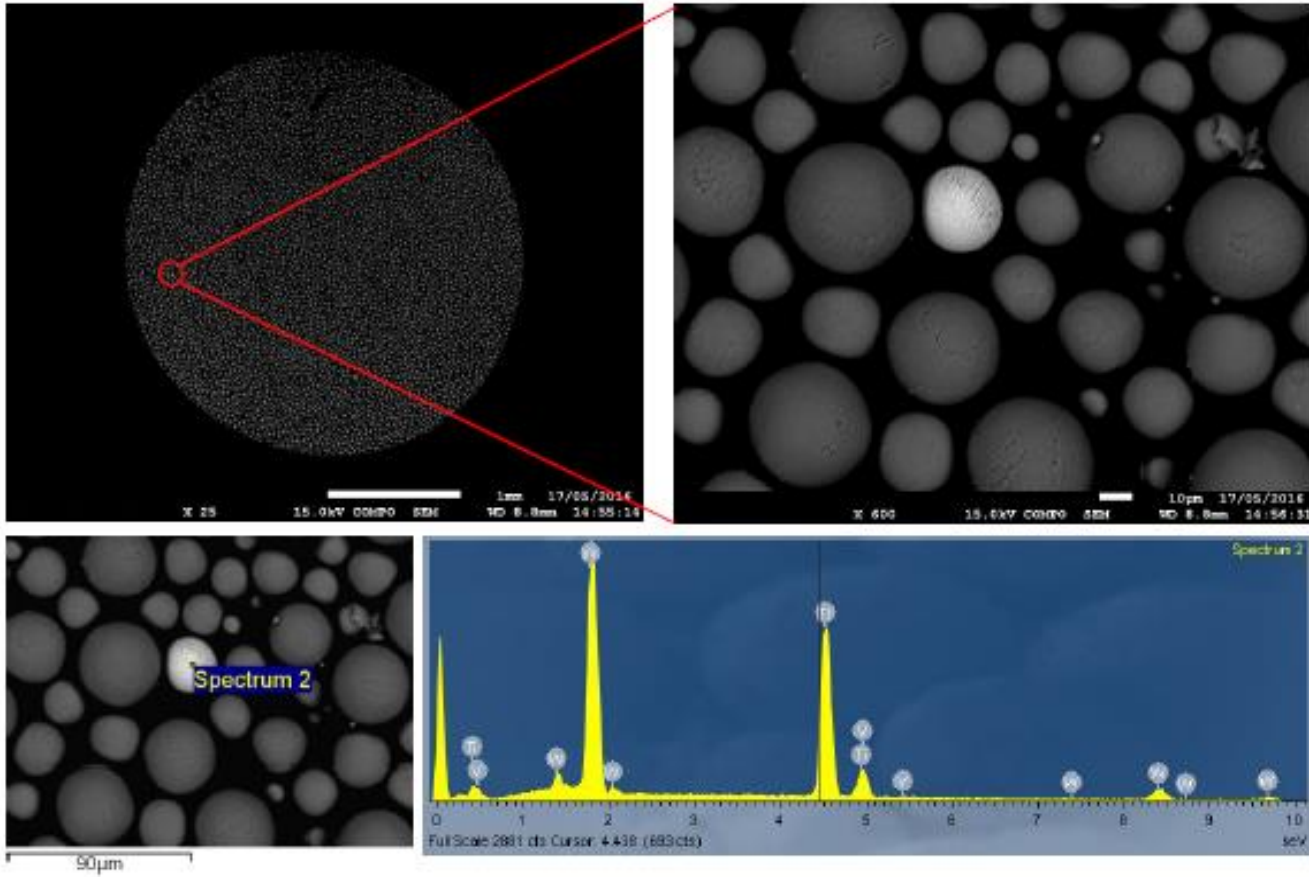


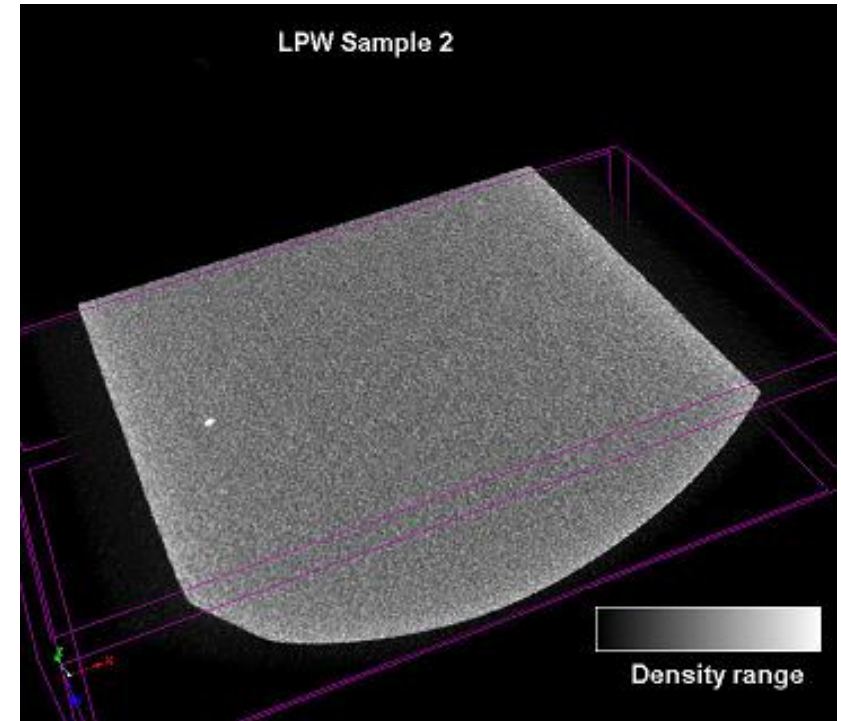
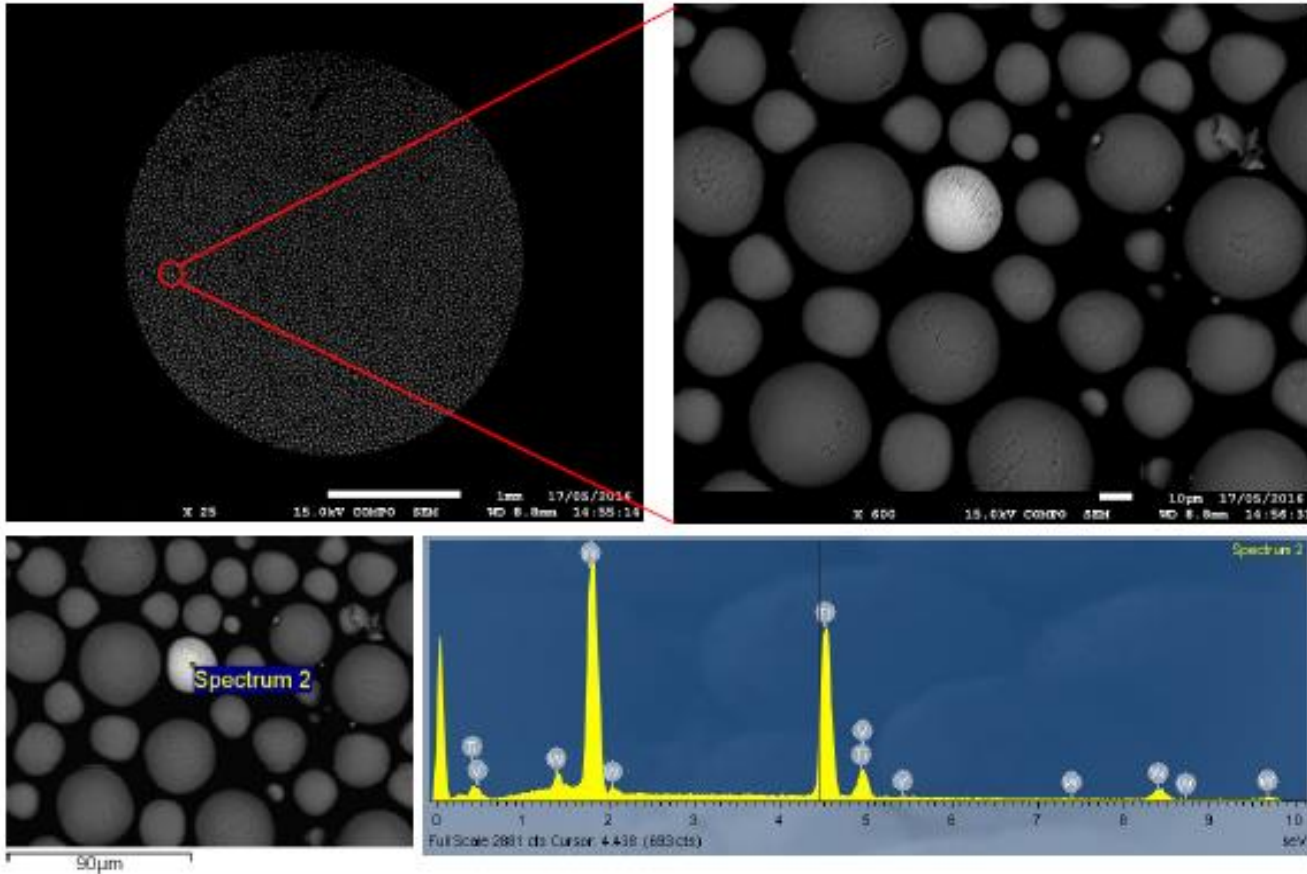
Our Locations



 LPW Technology  LPW reseller

Contamination – Devil Particle





1kg AM Powder \approx 2 Billion Particles \approx 18 sqm surface area



PowderLife Strategy

“Creating novel solutions and products that enable our customers to ensure quality, traceability, and consistency of powder during re-use within the AM process”

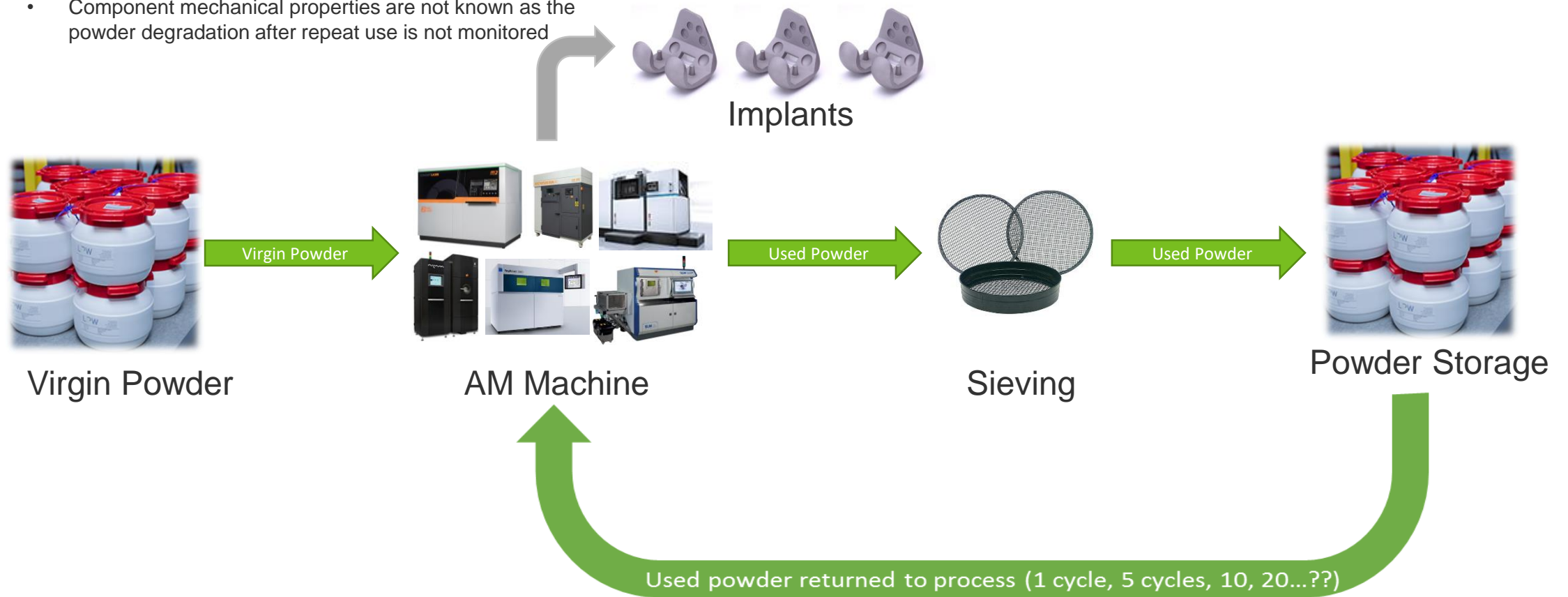
- Quality & Traceability
 - Application Teams → process mapping (powder handling & reuse methodologies)
 - **POWDERSOLVE** → fundamental backbone of all current and future TPM products & processes
- Contamination - control and measure “the devil particle”
 - Implement best practices powder handling & reuse methodologies
 - Reuse methodologies based on experimental data
 - Test certification focused on contamination & statistical confidence through repeated sampling



In-process Powder Control

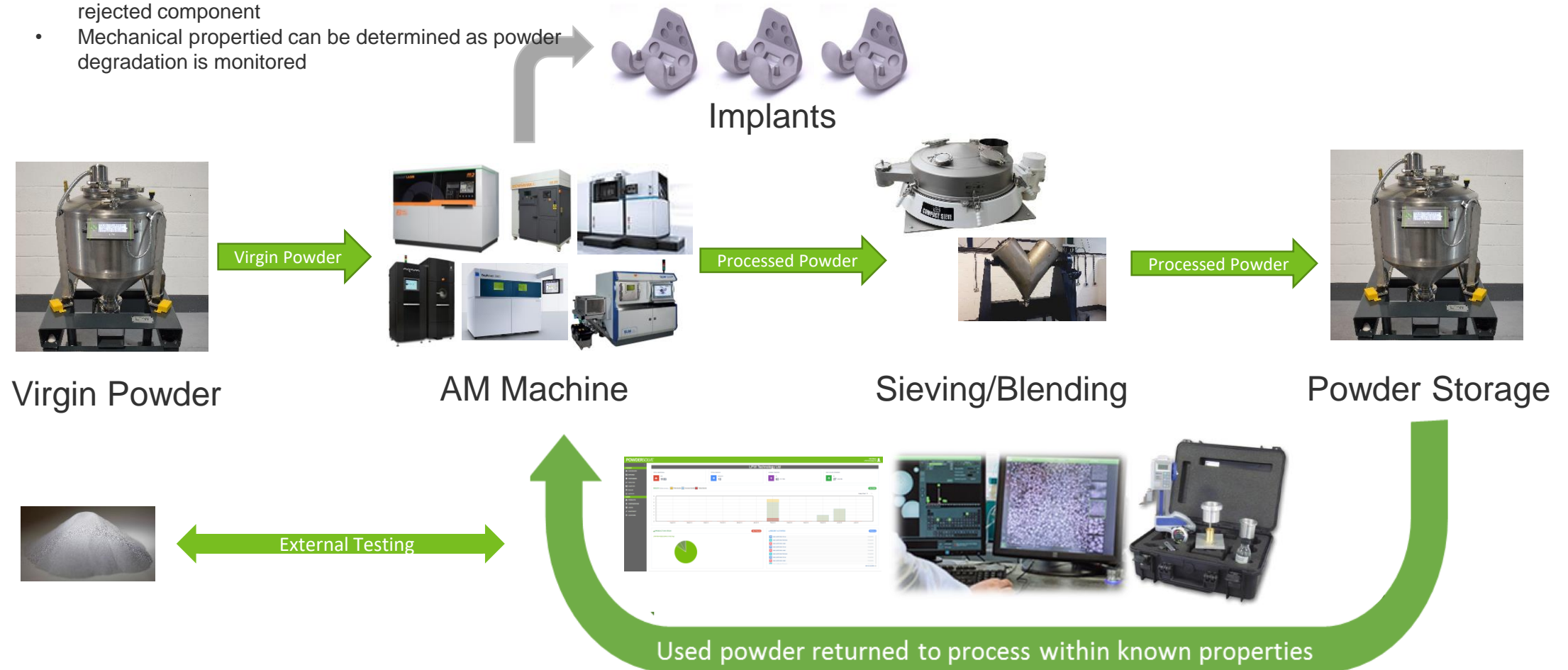
Traditional AM Powder Cycle

- Virgin powder and recycled powder used to manufacture
- Traceability of the powder lost after 1st build
- Impossible to operate an effective product recall system
- Component mechanical properties are not known as the powder degradation after repeat use is not monitored



Traditional AM Powder Cycle

- The blending of virgin and used powders are controlled
- Full traceability of all raw materials is maintained – possible to implement an effective product recall in the event of a rejected component
- Mechanical properties can be determined as powder degradation is monitored

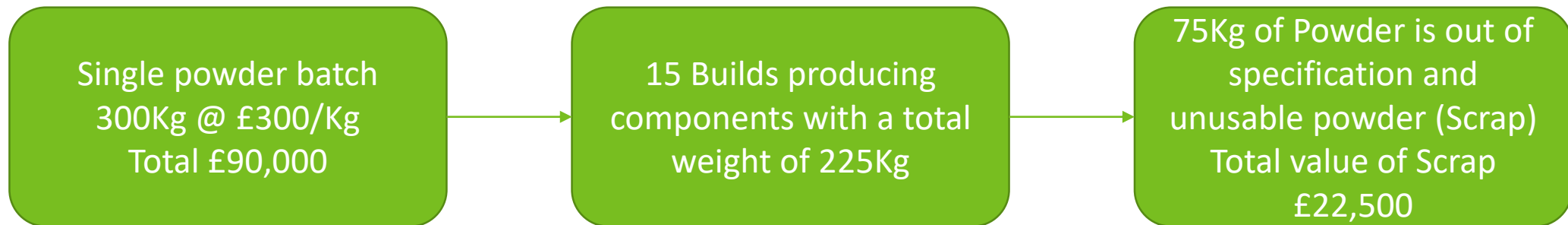




Impact of In-process Powder Control

Cost Savings

- Requirement for 450,000 components over 25 years
- 15 builds per powder batch
- 10 component per build
- 15 builds per machine per month





Impact of In-process Powder Control

Manufacture of production components

CURRENT COST

• 15 builds per month on one machine	Input	£90K	Scrap	£22.5K
• Monthly requirements for 10 machines	Input	£900K	Scrap	£225K
• Annual powder requirements for 10 machines	Input	£10.8M	Scrap	£2.7M
• Powder required for the complete project life cycle	Input	£270M	Scrap	£67.5M



Impact of In-process Powder Control

Manufacture of production components

- Increase powder usage by 1 build per batch
 - Total powder requirements reduce by £16.8M
 - Scrap powder reduced by £4.21M
- Impact on component costs during lifetime of project
 - Initial cost per part £600
 - Increase powder usage £562.5 (6% cost reduction)



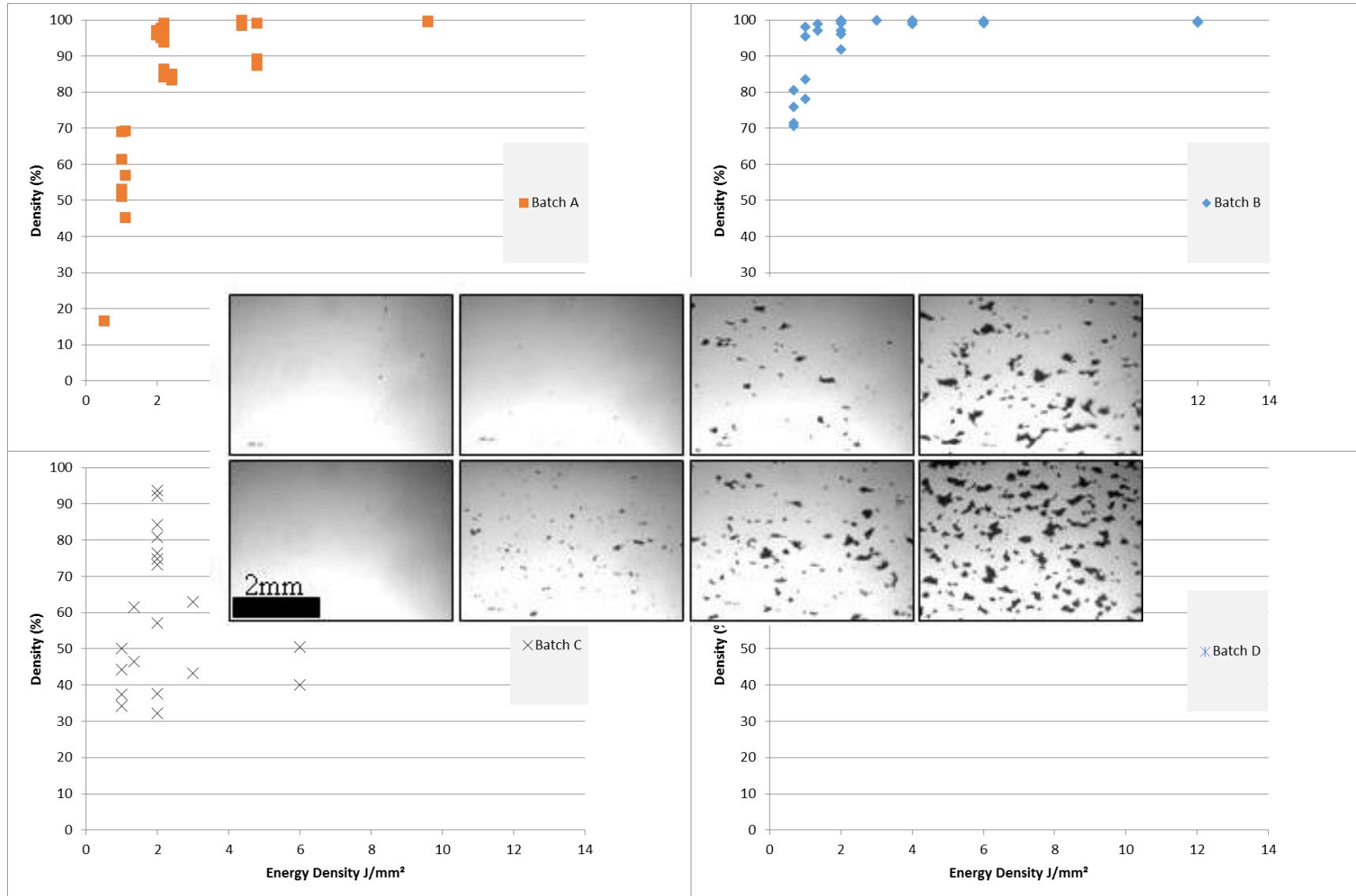
Case Study – AM Processing Window and Supplier Evaluation

Importance of powder specifications



Case Study – AM Processing Window and Supplier Evaluation

Importance of powder specification



- Supply chain stability – dual atomisation source for all core products
- Powder batches with 15-45micron size range
- Variable scatter and success in AM build quality
- Caution! Energy Density!!



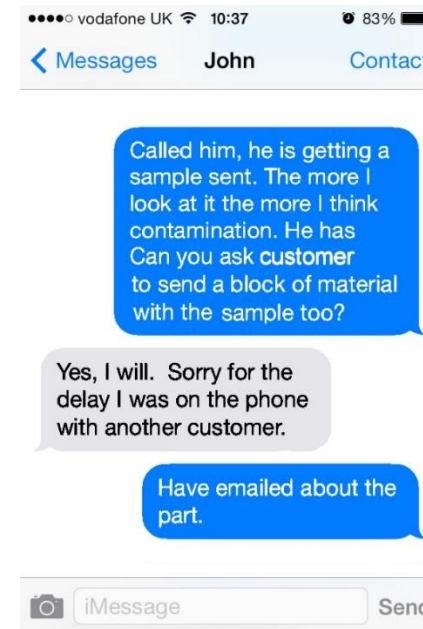
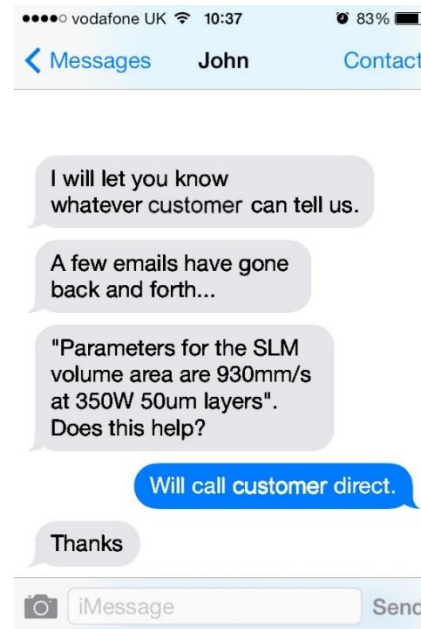
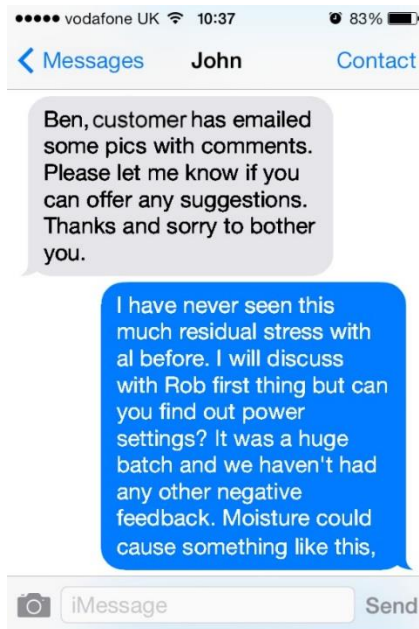
Case Study – The Devil Particle



Aluminium Contamination

Monday 25th August - Problem

- Customer informs that their aluminium products have failed and suspect problem with the powder
- Text messages show Ben and John making a start on resolving the issue put forward by the customer



Case Study – Aluminium Contamination

Tuesday 26th August - Problem

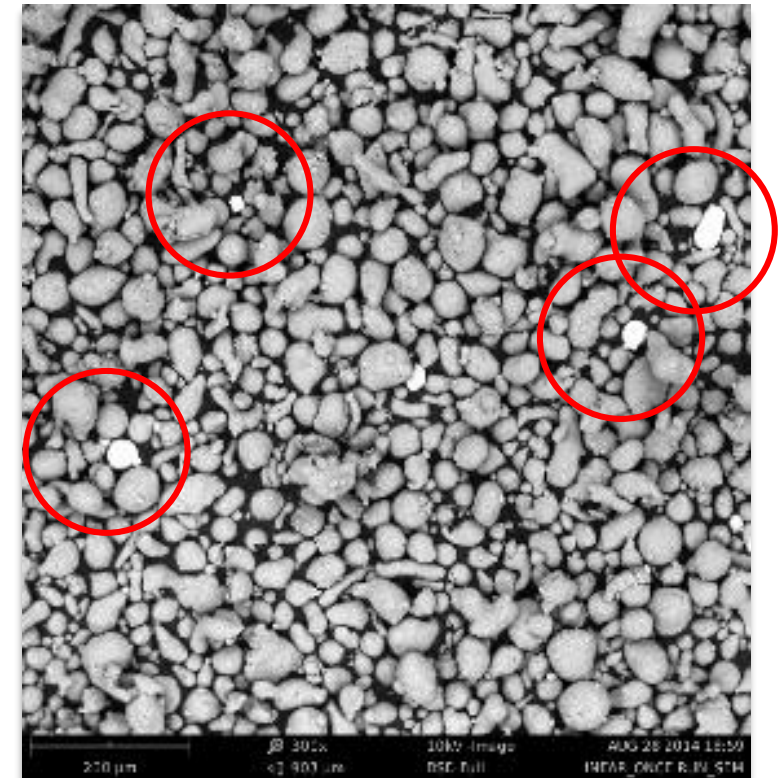
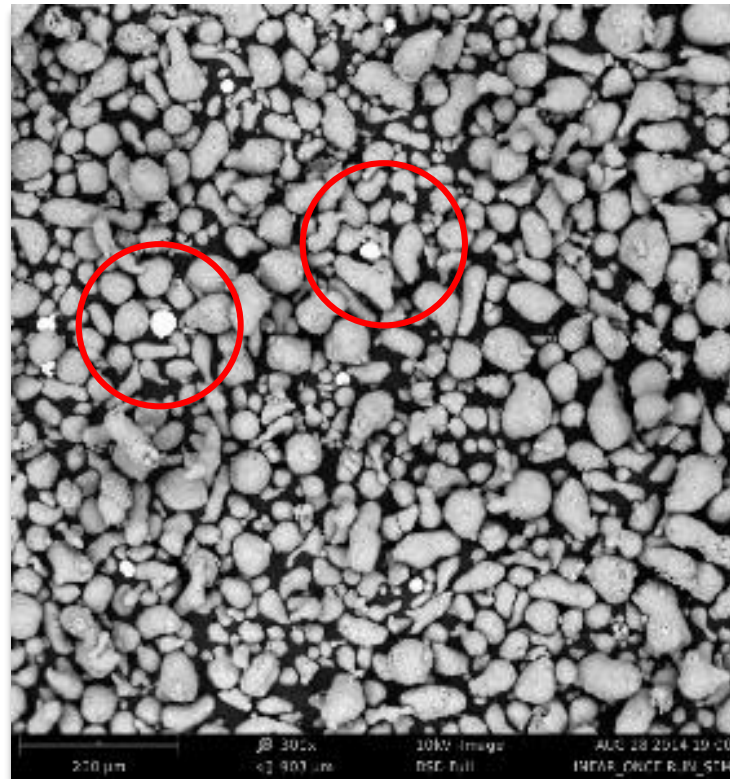
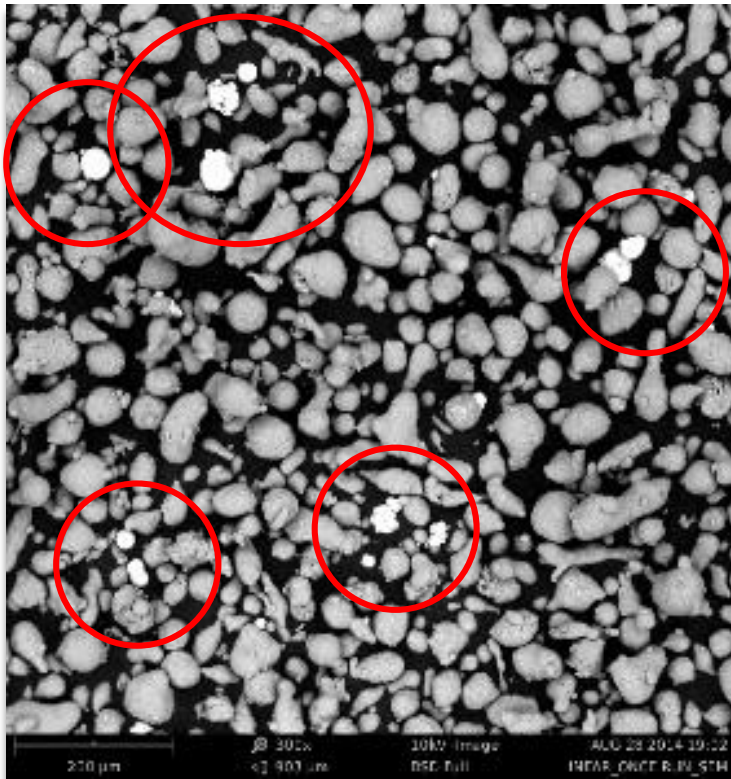
- Failed aluminium parts



Case Study – Aluminium Contamination

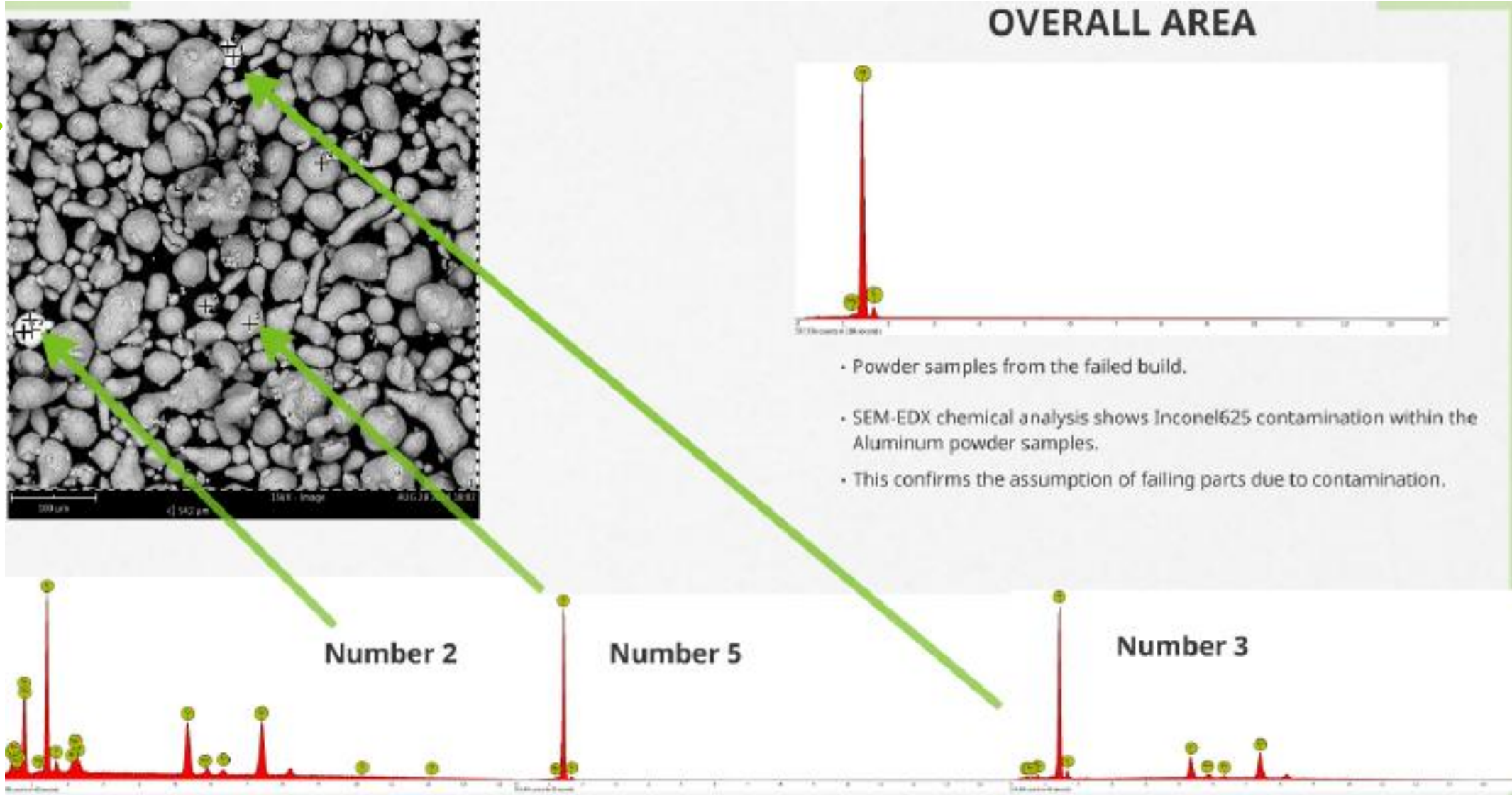
Thursday 28th August - Testing

- Powder samples from failed build
- This confirms that there is some degree of contamination but is not conclusive that this level of contamination can cause cracking



Case Study – Aluminium Contamination

Thursday 28th August - Testing

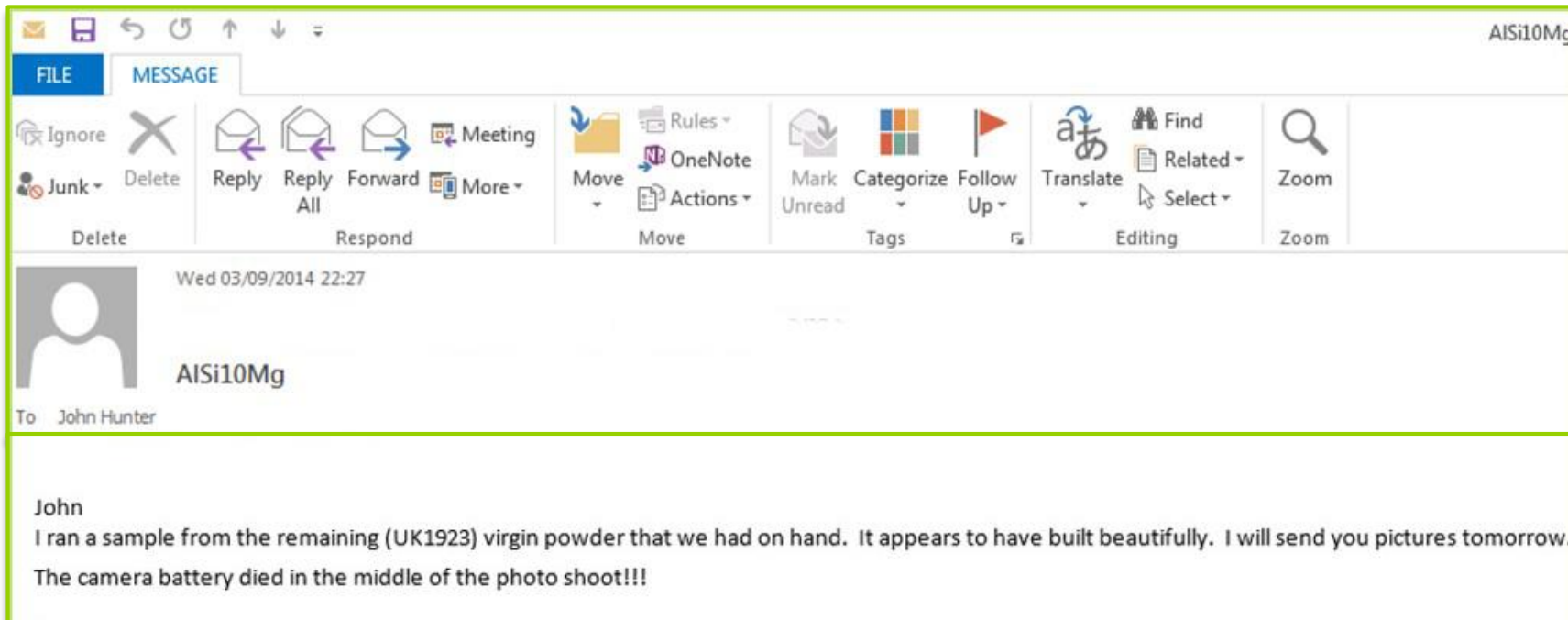




Case Study – Aluminium Contamination

Wednesday 3rd September - Solution

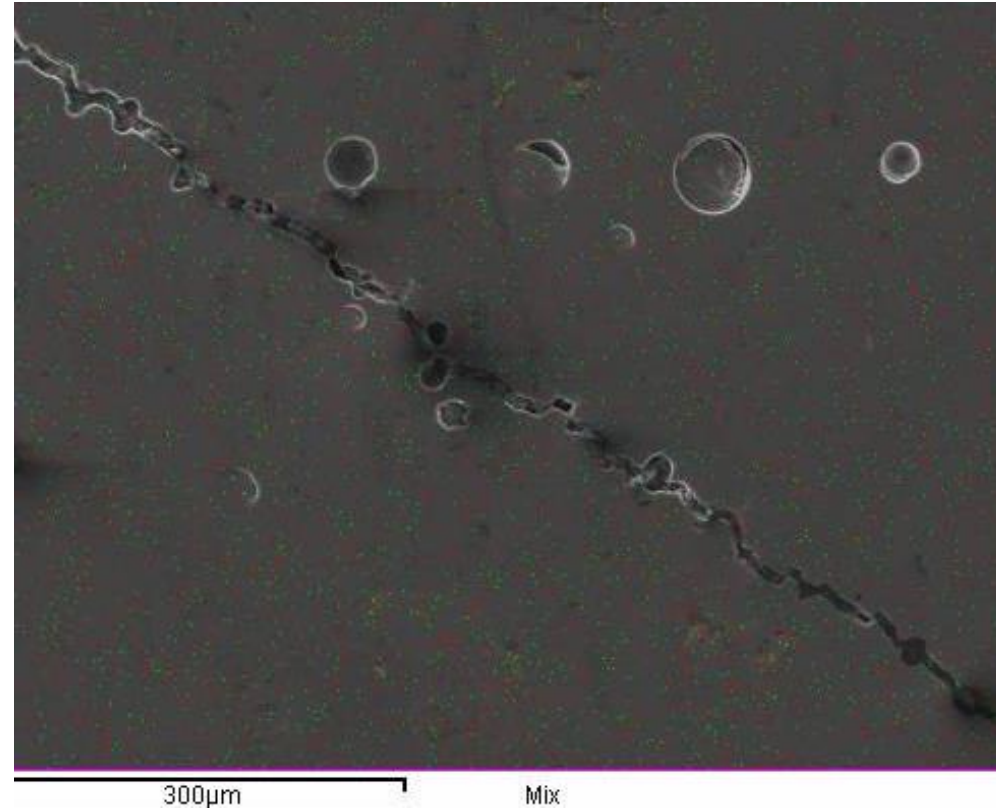
- Testing confirms powder was contaminated
- Using the virgin powder for the product gave a product that was “built beautifully”



Case Study – Aluminium Contamination

Validation

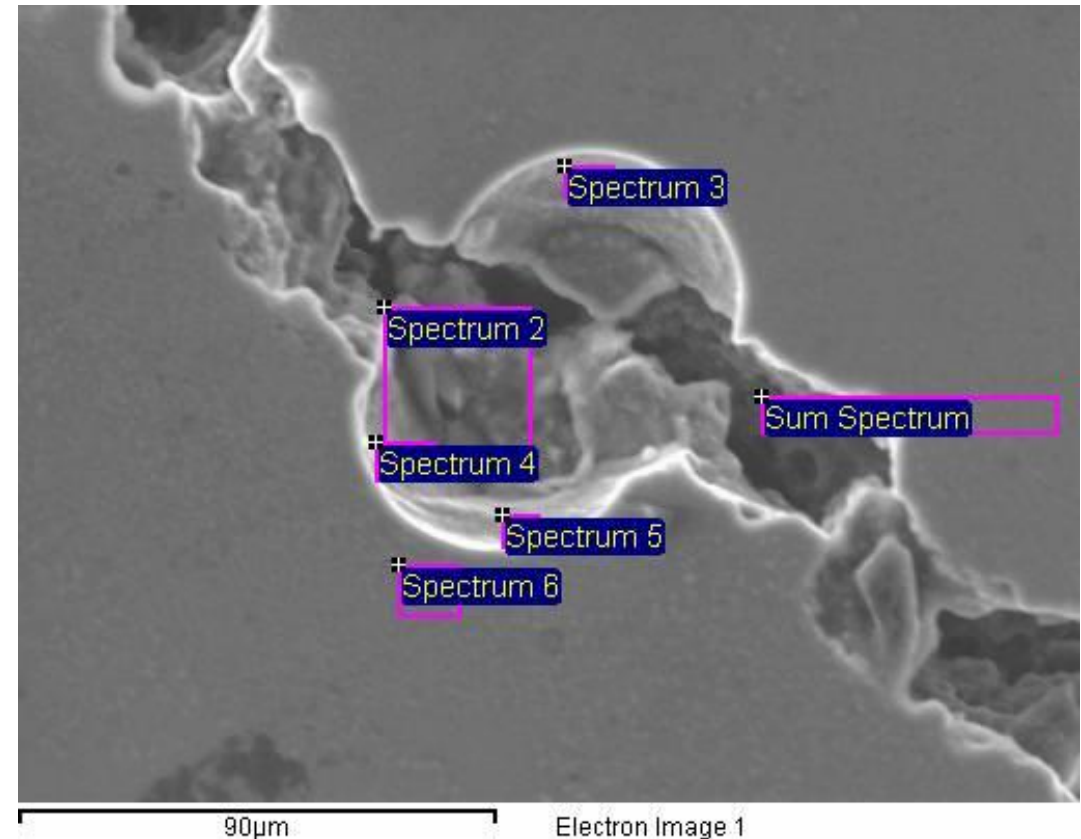
Element	Weight%	Atomic%
Al	81.93	85.51
Si	10.93	10.96
Cr	1.72	0.93
Ni	5.42	2.60
Totals	100.00	100.00



Nickel homogeneously spread in the aluminium matrix

Spectrum	Al wt%	Si wt%	Cr wt%	Ni wt%	Total
SumSpectrum	79.55	12.63	1.79	6.03	100.00
Spectrum 2	48.05	5.37	6.30	40.28	100.00
Spectrum 3	58.87	8.61	4.38	28.14	100.00
Spectrum 4	58.30	11.22	3.31	27.16	100.00
Spectrum 5	76.13	16.04	2.27	5.57	100.00
Spectrum 6	81.56	10.24	1.98	6.22	100.00

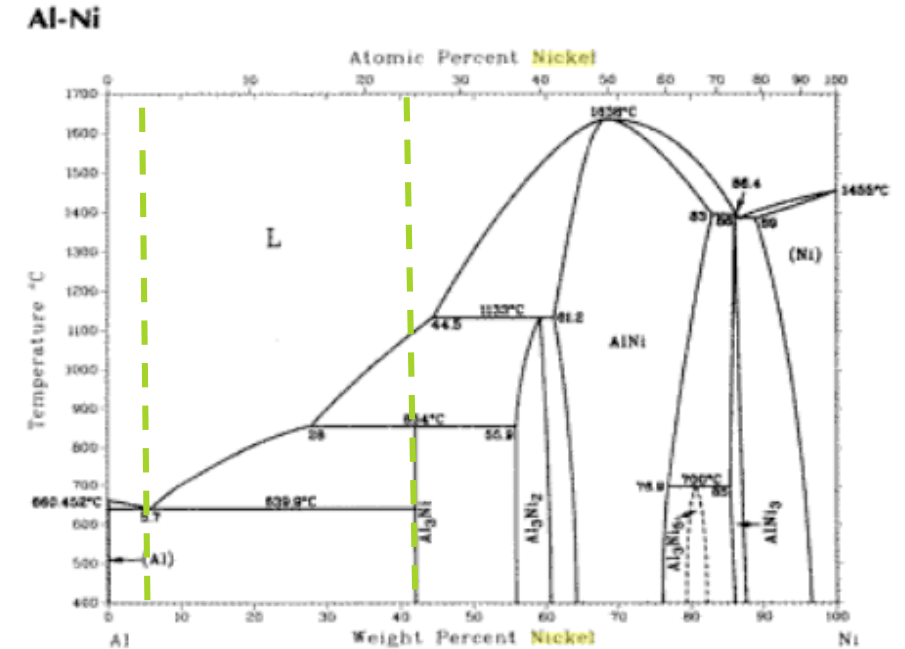
- At some points nickel content is relatively high
- Phase diagram would suggest high volume percent of brittle intermetallic phases in the Al matrix
- Nickel content could be even higher at some points, but due to the crack Al noise could be measured from different planes



Case Study – Aluminium Contamination

Solution - Physical Metallurgy: AL – NI Binary Diagram

- Ni solubility in Al is limited to 0.24 wt%
 - Not contributing to matrix strengthening
- Over solubility limit Ni starts to appear as an insoluble intermetallic (NiAl_3) increasing the strength
 - Usually up to 4 wt% Ni is used
- NiAl_3 volume percent increases with Ni content
- In the hypoeutectic (<5.7 wt%) Ni starts to appear as interdendritic α Al – NiAl_3 eutectic
- In the hypereutectic (>5.7 wt%) Ni appears as large NiAl_3 particles which are detrimental for ductility
- Over ~ 42 % more brittle intermetallic phases are starting to appear in the Al matrix
- The most brittle are the AlNi (61-83 wt%) and NiAl_3 (85-87 wt%)
 - Also known as nickel aluminides – potential for high temperature structural applications, but with almost 0% ductility



P. Nash, M.F. Singleton, and J.L. Murray, 1991

Phase	Composition, wt% Ni	Pearson symbol	Space group
(Al)	0 to 0.24	<i>cF4</i>	<i>Fm$\bar{3}m$</i>
Al_3Ni	42	<i>oP16</i>	<i>Pnma</i>
Al_3Ni_2	55.9 to 60.7	<i>hP5</i>	<i>P$\bar{3}m1$</i>
AlNi	61 to 83.0	<i>cP2</i>	<i>Pm$\bar{3}m$</i>
Al_3Ni_5	79 to ~82	...	<i>Cmmm</i>
AlNi_3	85 to 87	<i>cP4</i>	<i>Pm$\bar{3}m$</i>
(Ni)	89.0 to 100	<i>cF4</i>	<i>Fm$\bar{3}m$</i>



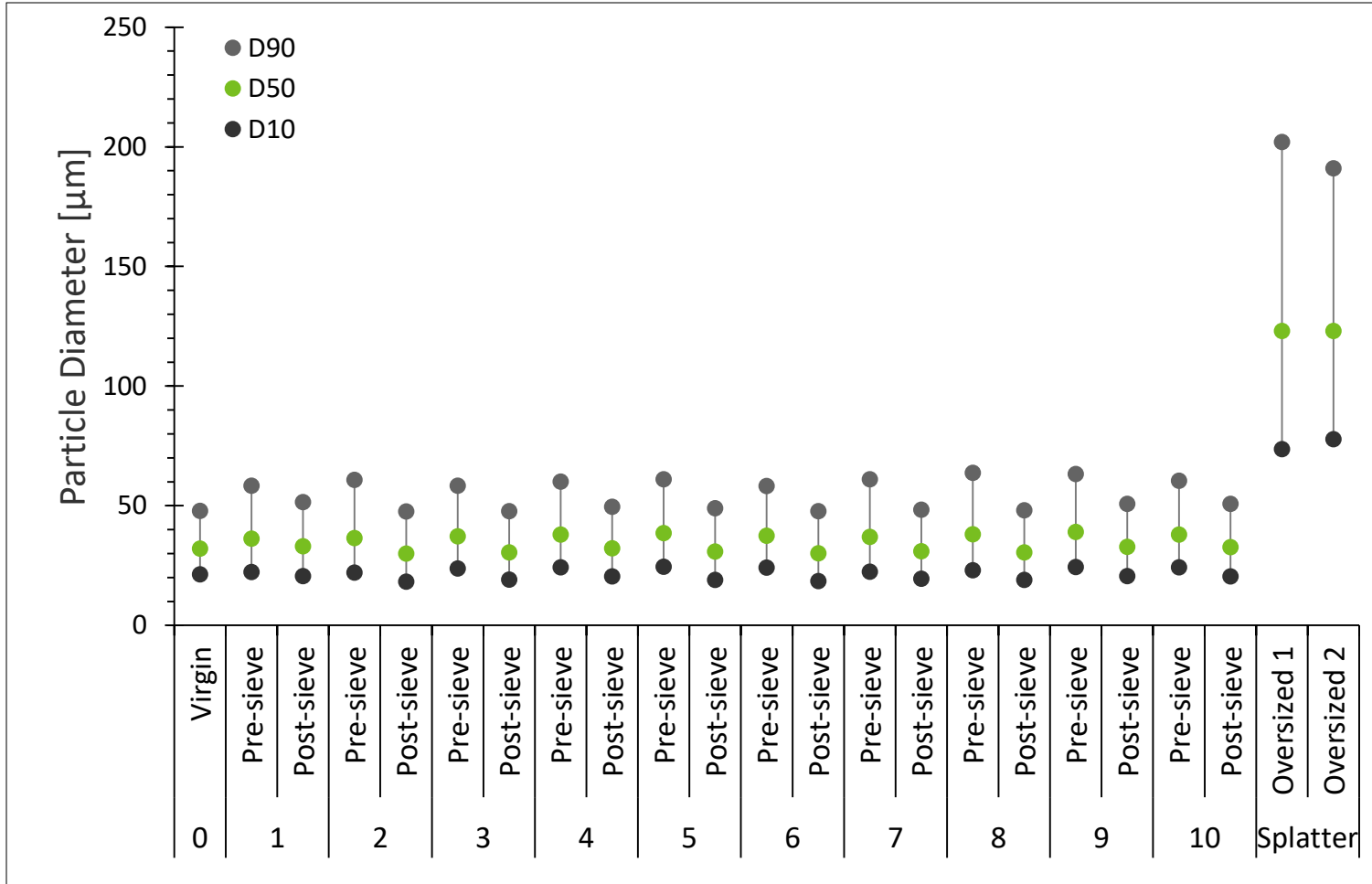
Degradation of Ti-6Al-4V Powder in Powder Bed Fusion

Can you re-use powder which has been through AM process?



Degradation of Ti-6Al-4V Powder

Particle Size Distribution

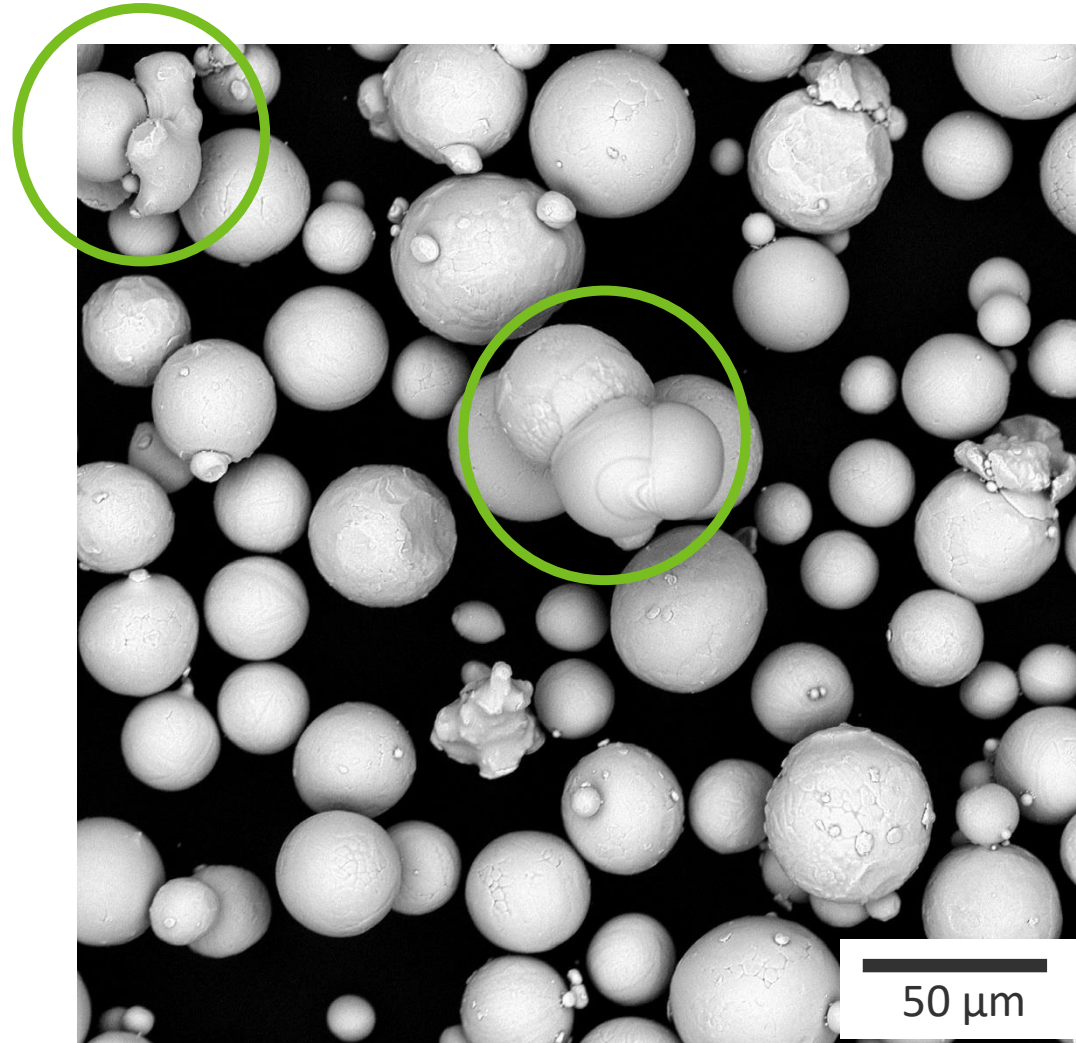


- Range of powder sizes
- Particle size and distribution tends to increase after a build
 - Sieving brings size and range closer to virgin
- Oversized particles have the largest diameter and have the largest range

Degradation of Ti-6Al-4V Powder

Powder Shape

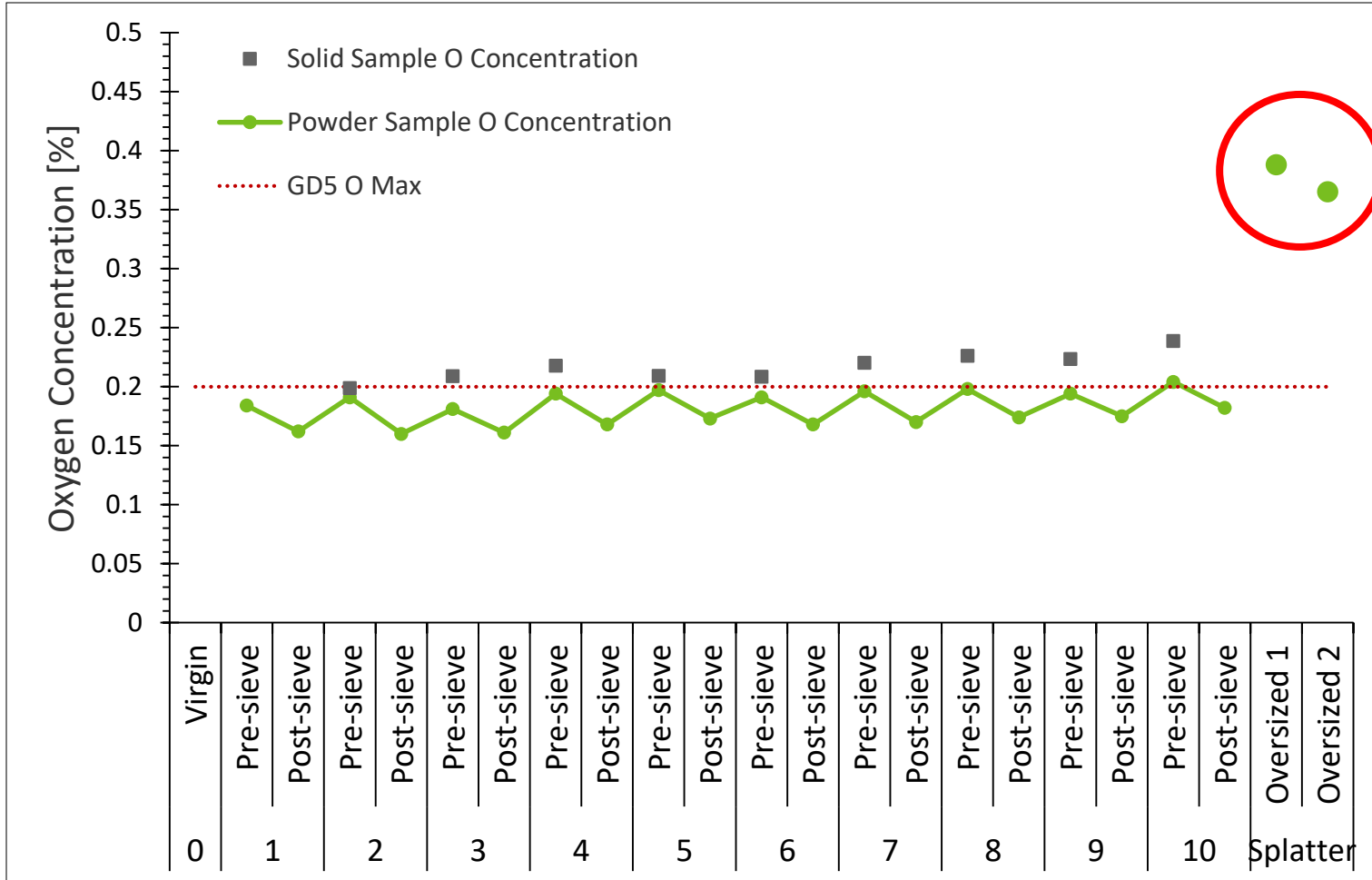
- Oversized irregular particles and agglomerates from Spatter





Degradation of Ti-6Al-4V Powder

Powder Chemistry - Oxygen

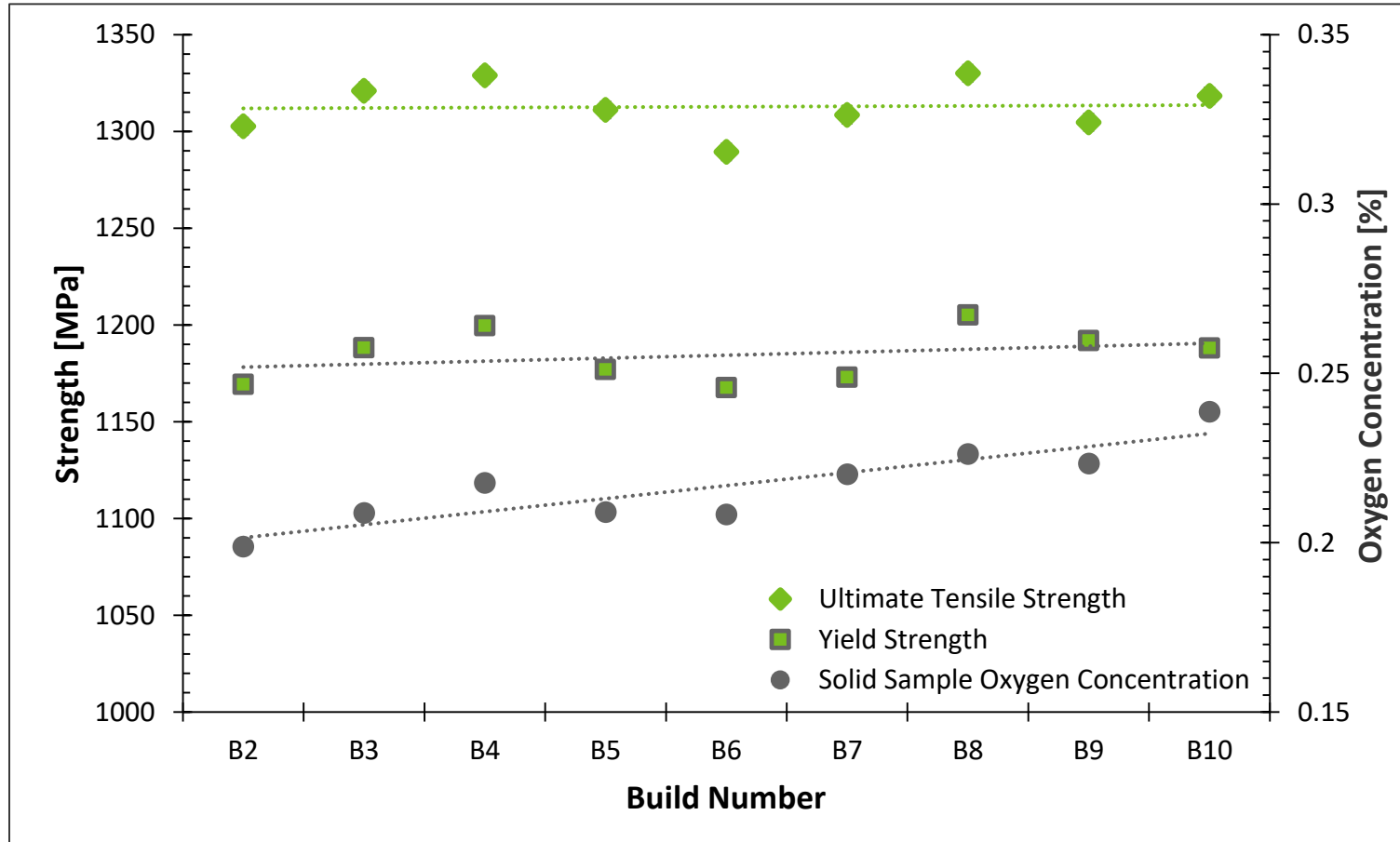


- Oxygen content has an influence on the final part's mechanical properties
- Oxygen increase after first build
- Sieving out large particles significantly decreases oxygen content
- General increase with more builds
- Remains Grade 5 specification until build 10
- Oversized particles have largest oxygen content
- Oxygen content in solid sample slightly higher than powder



Degradation of Ti-6Al-4V Powder

Mechanical Properties - Strength

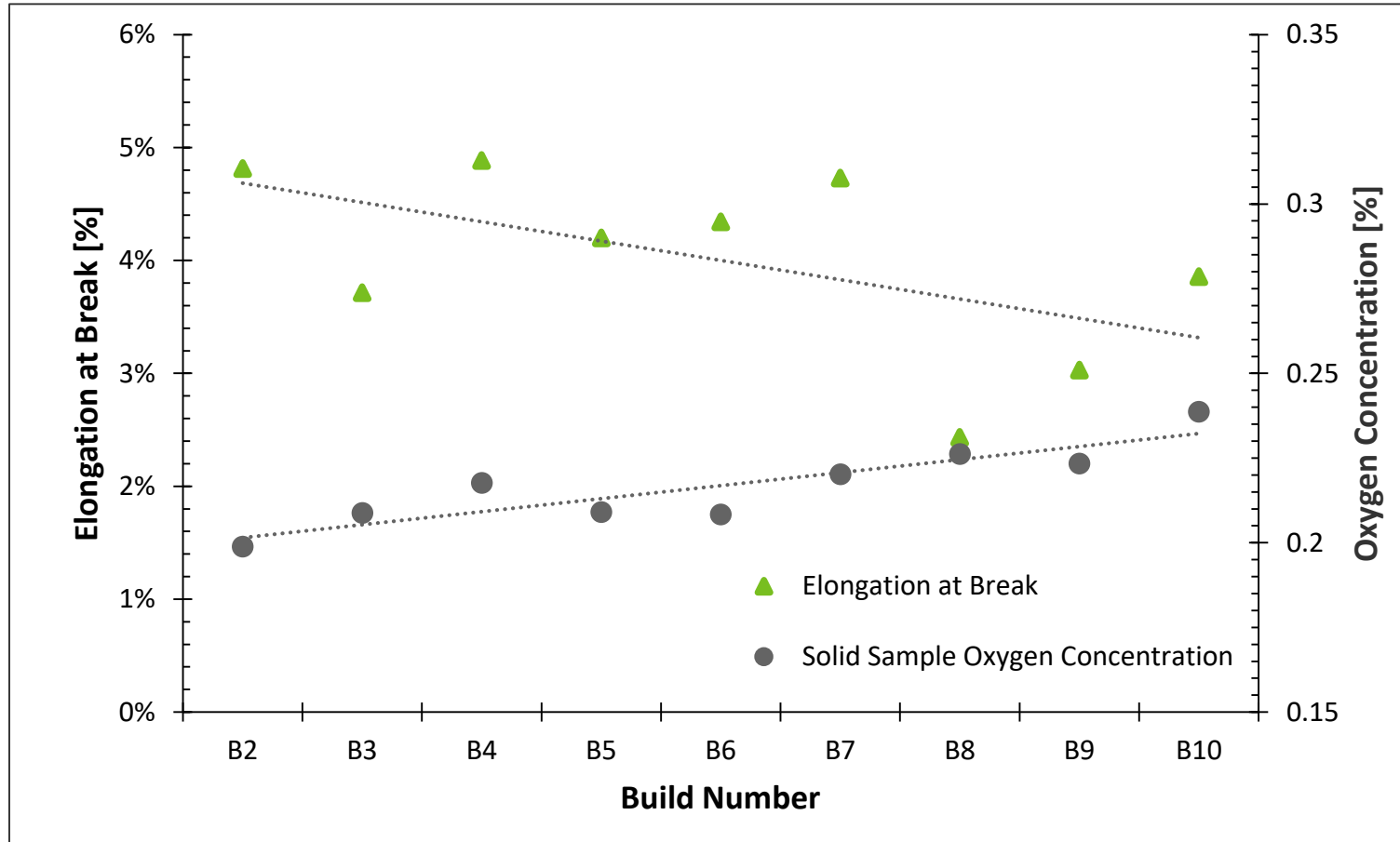


- As-build part strength properties stay relatively unchanged from Build 1 to Build 10
- Yield strength and ultimate tensile strength heavily correlated with oxygen content



Degradation of Ti-6Al-4V Powder

Mechanical Properties - Ductility



- Ductility has decreasing trend with build number
- Ductility in AM influenced by:
 - Porosity
 - Impurity content
- Ductility has is heavily correlated to oxygen content in present study



Degradation of Ti-6Al-4V Powder

Summary

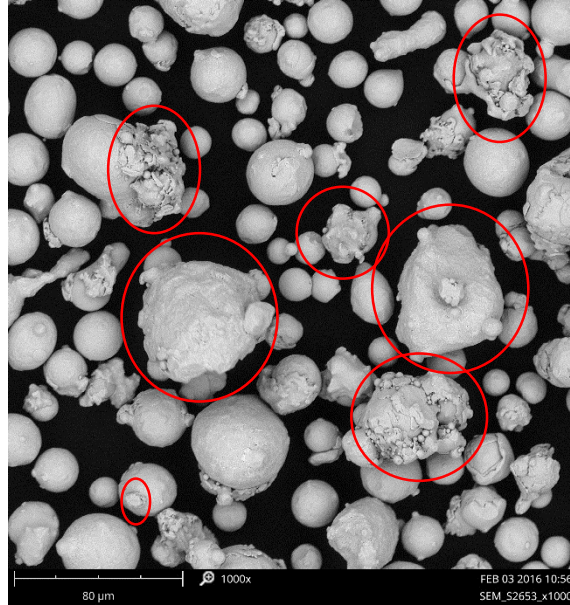
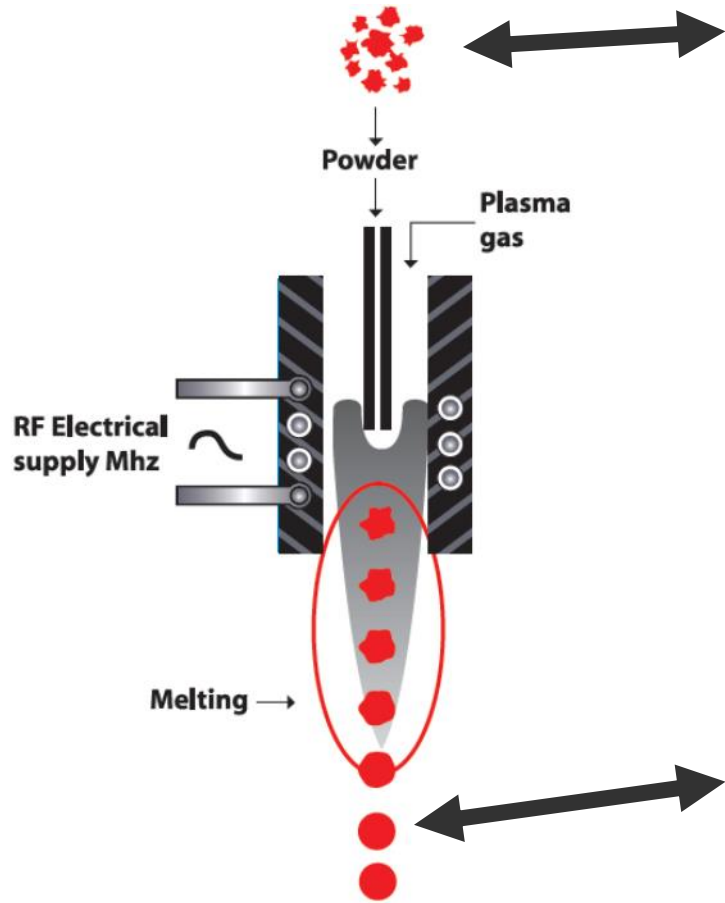
- Powder is effected from reuse
 - Oxygen and Nitrogen content increase
 - Powder became more spherical (aspect ratio increased)
- Powder is effected by post-process sieving
 - Removes large agglomerates that are high in oxygen and nitrogen
- Porosity in built part increases when using recycled powder
- Variation in mechanical strength with reuse
 - High correlation with oxygen content
- Ductility degrades with reuse
 - High correlation with oxygen content
 - Increased porosity could be contributing factor



Concluding remarks

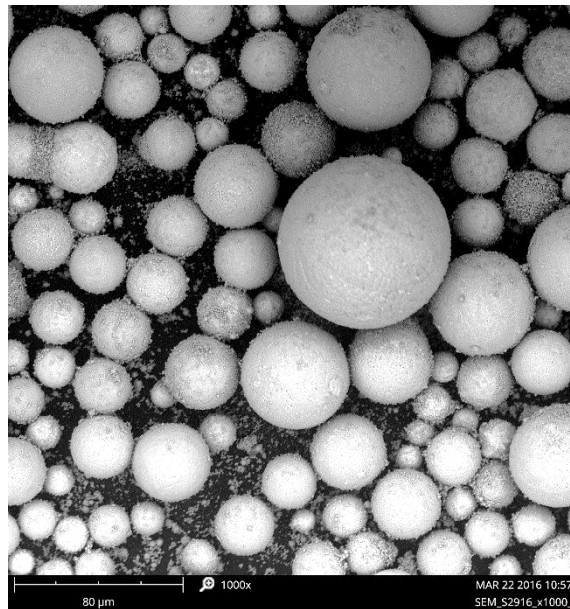
- Three case studies presented
 - Importance of **Powder Specification**
Variability between suppliers
 - **Contamination** can be catastrophic
Measures to detect and mitigate must be employed
 - Powder changes (**Degradation**) with repeated use
Critical to high-end applications and must be managed and understood to ensure traceability is maintained

LPW- 247LC Plasma Spheroidisation



As-Atomised feedstock

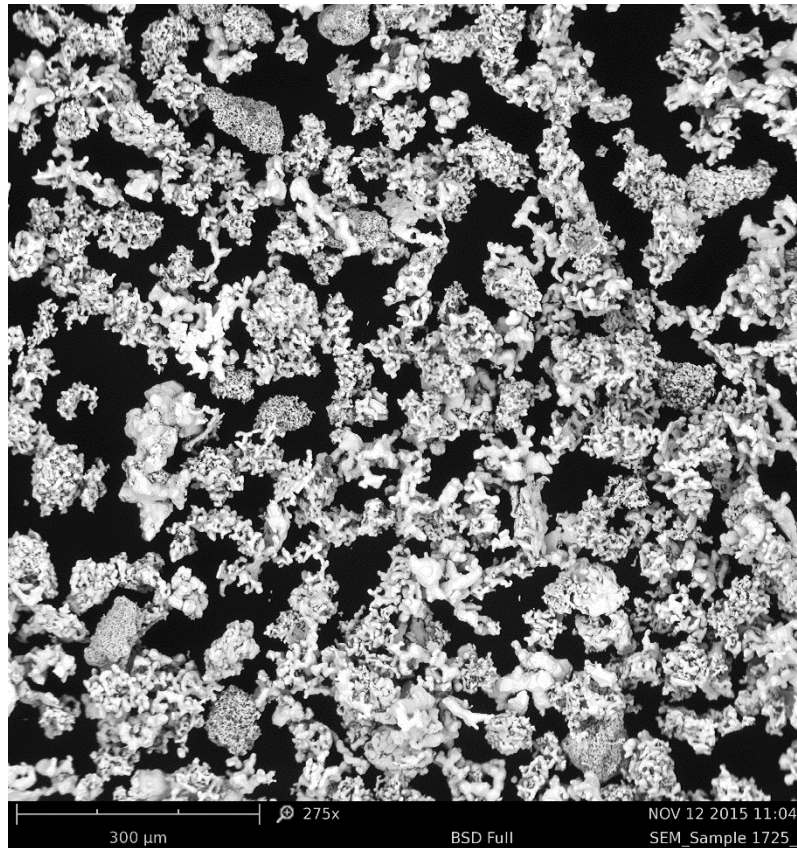
- Poor flow
- High surface area
- High O & N content



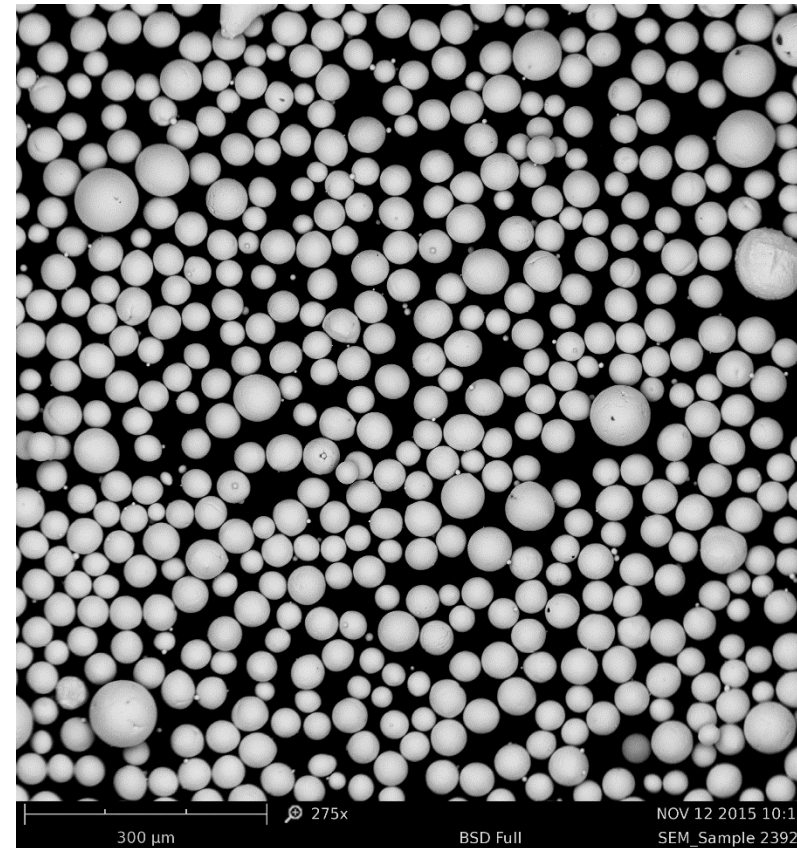
Plasma Spheroidised

- Enhanced flow
- Reduced surface area
- Removal of organic contamination
- Lower O & N content

As- received feedstock



Plasma Spheroidised





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